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## BENDING STRENGTH OF BEVEL GEARS

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### PRODUCT CATEGORY

#### SPUR GEARS

#### HELICAL GEARS

#### INTERNAL GEARS

#### GEAR RACK

#### CP RACKS & PINIONS

#### MITER GEARS

#### BEVEL GEARS

#### SCREW GEARS

#### WORM GEAR

This information is valid for bevel gears which are used for power transmission in general industrial machines. The applicable ranges are:

Transverse module / m / 1.5 – 25mm

Pitch diameter / d<sub>0</sub> / 1600mm or less (for straight bevel gears), 1000mm or less (for spiral bevel gears)

Tangential speed / v / 25m/s or less

Rotational speed / n / 3600rpm or less

### (1) Conversion Formulas

In calculating strength, transmitted tangential force at the pitch circle, F<sub>tm</sub> (kgf), power, P (kW), and torque, T (kgf · m), are the design criteria. Their basic relationships are expressed in the following Equations.

$$F_{tm} = \frac{102P}{v_m} = \frac{1.95 \times 10^6 P}{d_m n} = \frac{2000T}{d_m} \quad (10.27)$$

$$P = \frac{F_{tm} v_m}{102} = 5.13 \times 10^{-7} F_{tm} d_m n \quad (10.28)$$

$$T = \frac{F_{tm} d_m}{2000} = \frac{974P}{n} \quad (10.29)$$

Where v<sub>m</sub>: Tangential speed at the central pitch circle (m/s)  
= d<sub>m</sub>n / 19100

## BEVEL GEARBOX

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### KHK GEAR MANUFACTURING PROCESS



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$$d_m: \text{ Central pitch diameter (mm)} \\ = d_0 - b \sin \delta_0$$

## (2) Bending Strength Equations

The tangential force,  $F_{tm}$ , acting at the central pitch circle should be less than the allowable tangential force,  $F_{tmlim}$ , which is based upon the allowable bending stress at the root  $\sigma_{Flim}$ .

That is:

$$F_{tm} \leq F_{tmlim} \quad (10.30)$$

The bending stress at the root,  $\sigma_F$ , which is derived from  $F_{tm}$  should not exceed the allowable bending stress  $\sigma_{Flim}$ .

$$\sigma_F \leq \sigma_{Flim} \quad (10.31)$$

The tangential force at the central pitch circle,  $F_{tmlim}$ (kgf) is obtained from Equation (10.32).

$$F_{tmlim} = 0.85 \cos \beta_m \sigma_{Flim} m b \frac{R_a - 0.5b}{R_a} \left. \frac{1}{Y_F Y_\epsilon Y_\beta Y_C} \left( \frac{K_L K_{FX}}{K_M K_V K_O} \right) \frac{1}{K_R} \right\} (10.32)$$

Where  $\beta_m$  : Mean spiral angle (degrees)

$m$  : Transverse module (mm)

$R_a$  : Cone distance (mm)

The bending strength at the root,  $\sigma_F$  (kgf/mm<sup>2</sup>), is calculated from Equation (10.33).

$$\sigma_F = F_{tm} \left. \frac{Y_F Y_\epsilon Y_\beta Y_C}{0.85 \cos \beta_m m b} \frac{R_a}{R_a - 0.5b} \left( \frac{K_M K_V K_O}{K_L K_{FX}} \right) K_R \right\} (10.33)$$

## (3) Determination of Various Coefficients

### (3)-1 Facewidth $b$

The term  $b$  is defined as the facewidth on the pitch cone. For the meshed pair, the narrower one is used for strength calculations.

(3)-2 Tooth Profile Factor,  $Y_F$ 

The tooth profile factor,  $Y_F$ , can be obtained in the following manner: Using Figures 10.8 and 10.9, determine the value of the radial tooth profile factor,  $Y_{F0}$ . And then, from Figure 10.7 obtain the correction factor,  $C$ , for axial shift. Finally, calculate  $Y_F$  by Equation 10.34.

$$Y_F = CY_{F0} \quad (10.34)$$

Should the bevel gear pair not have any axial shift, the tooth profile factor,  $Y_F$ , is simply  $Y_{F0}$ .

The equivalent number of teeth,  $z_v$ , and the profile shift coefficient,  $x$ , when using Figures 10.8 and 10.9 is obtainable from Equation (10.35).

$$\left. \begin{aligned} z_v &= \frac{z}{\cos \delta_0 \cos^3 \beta_m} \\ x &= \frac{h_k - h_{k0}}{m} \end{aligned} \right\} \quad (10.35)$$

Where

$h_k$  : Addendum at outer end(mm)

$h_{k0}$  : Addendum of standard form(mm)

$m$  : Transverse module(mm)

$s$  : Outer transverse circular tooth thickness(mm)

The axial shift factor,  $K$ , is computed from the formula:

$$K = \frac{1}{m} \left\{ s - 0.5\pi m - \frac{2(h_k - h_{k0}) \tan \alpha_n}{\cos \beta_m} \right\} \quad (10.36)$$

Fig.10.7 Correction factor for axial shift, C

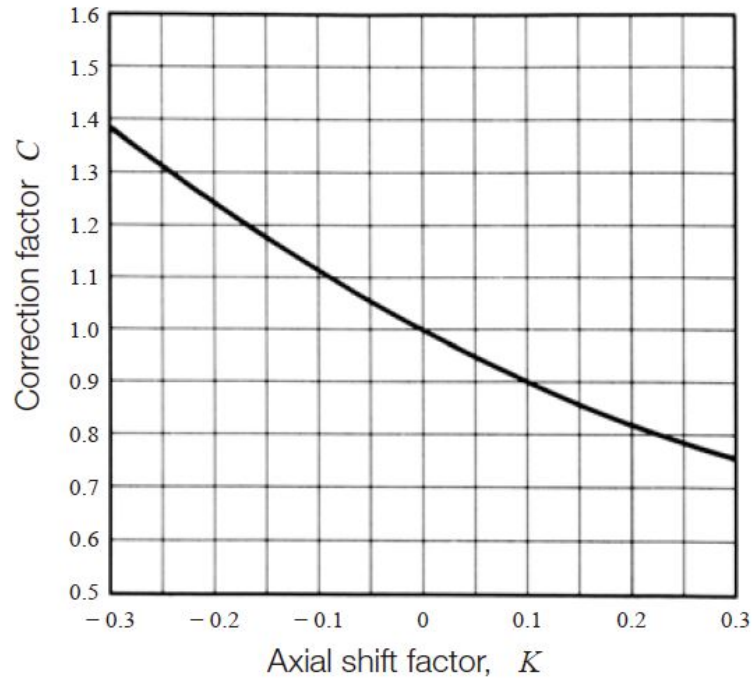


Fig.10.8 Tooth profile factor,  $Y_{Fa}$  (Straight bevel gear)

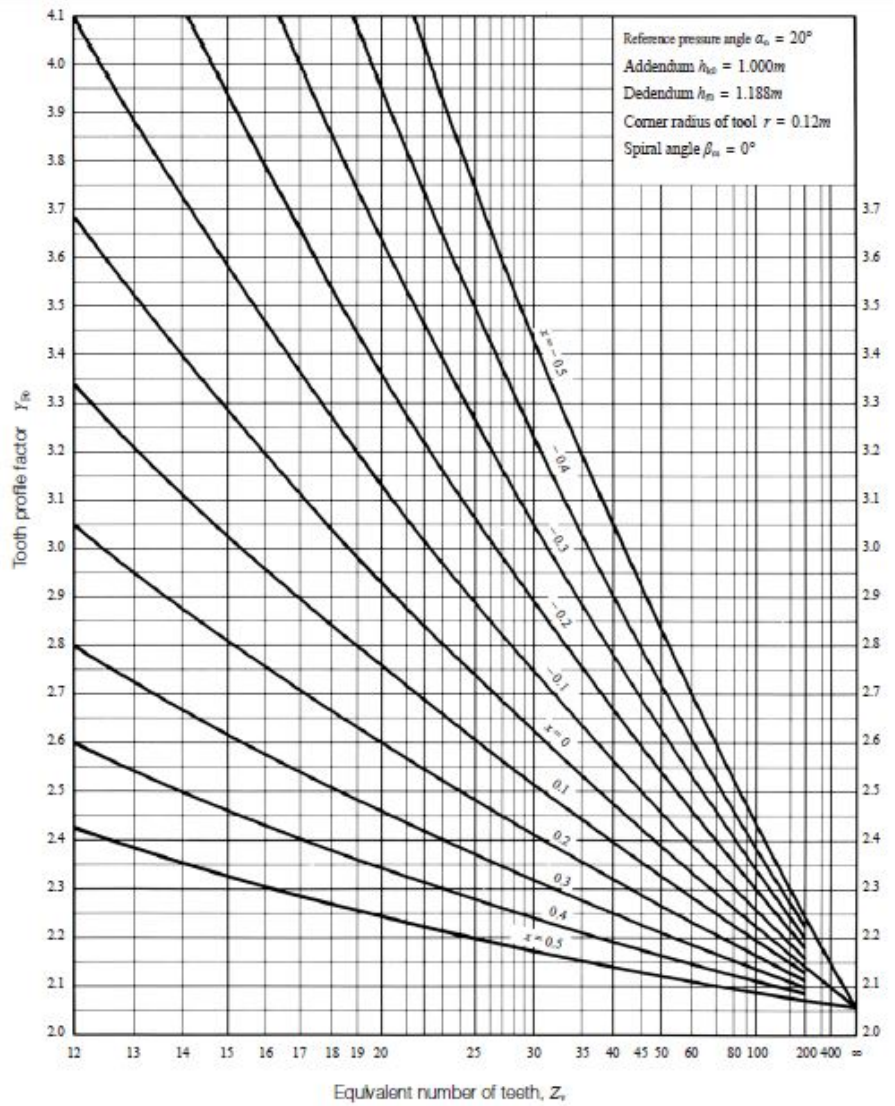
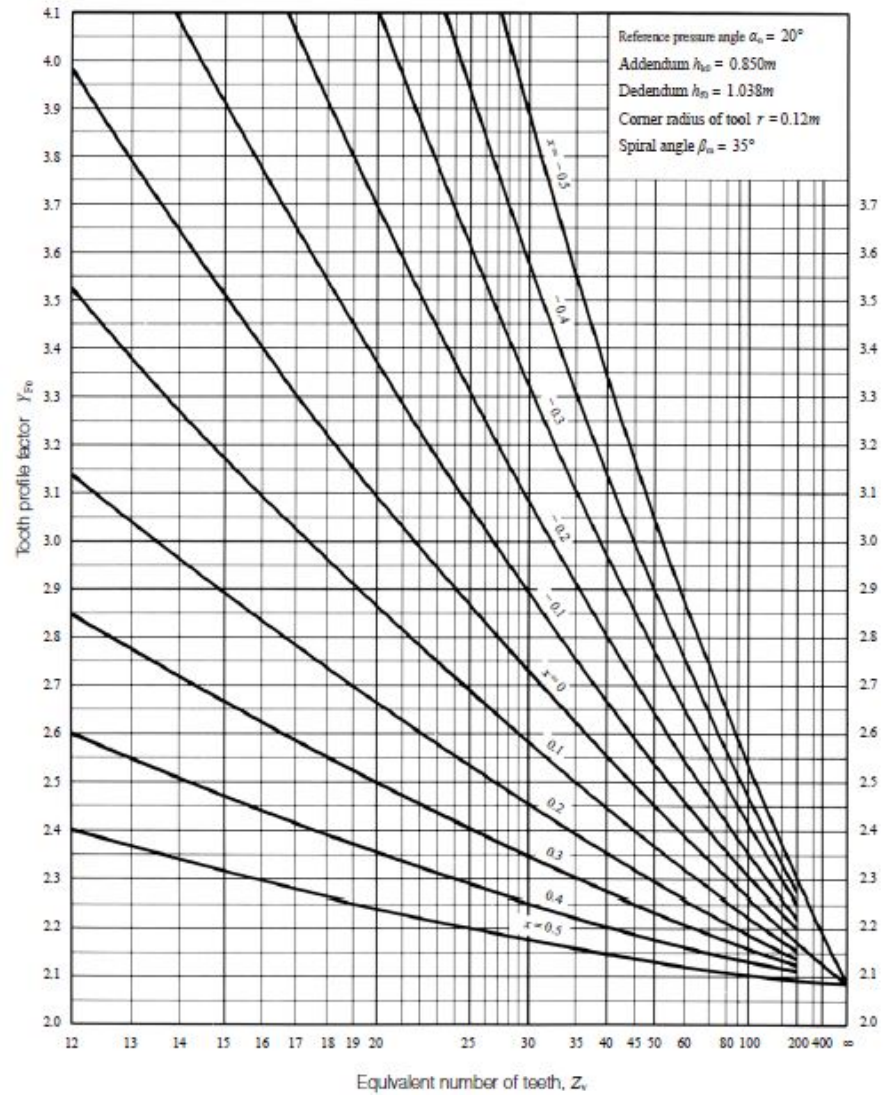


Fig.10.9 Tooth profile factor, YF0 (Spiral bevel gear)

(3)-3 Load Sharing Factor,  $Y_\varepsilon$ 

Load sharing factor,  $Y_\varepsilon$ , is the reciprocal of transverse contact ratio,  $\varepsilon_\alpha$ .

$$Y_\varepsilon = \frac{1}{\varepsilon_\alpha} \quad (10.37)$$

The transverse contact ratio,  $\varepsilon_\alpha$ , for a straight bevel gear mesh is:

$$\varepsilon_\alpha = \frac{\sqrt{R_{vk1}^2 - R_{vg1}^2} + \sqrt{R_{vk2}^2 - R_{vg2}^2} - (R_{v1} + R_{v2}) \sin \alpha_0}{\pi m \cos \alpha_0}$$

And the transverse contact ratio for spiral bevel gear is:

$$\varepsilon_\alpha = \frac{\sqrt{R_{vk1}^2 - R_{vg1}^2} + \sqrt{R_{vk2}^2 - R_{vg2}^2} - (R_{v1} + R_{v2}) \sin \alpha_s}{\pi m \cos \alpha_s} \quad (10.38)$$

See Tables 10.17 – 10.19 for some calculating examples of transverse contact ratio for various bevel gear pairs.

Where:

$R_{vk}$  : Tip diameter on back cone for equivalent spur gear (mm)

$$Rvk = Rv + hk = r_0 \sec \delta_0 + hk$$

$Rvg$  :Reference radius on back cone for equivalent spur gear(mm)

Helical gears  $= Rv \cos \alpha_0 = r_0 \sec \delta_0 \cos \alpha_0$

Spiral bevel gears  $= Rv \cos \alpha_s = r_0 \sec \delta_0 \cos \alpha_s$

$Rv$  :Back cone distance(mm)  $= r_0 \sec \delta_0$

$r_0$  :Pitch radius(mm)  $= 0.5z m$

$hk$  :Addendum at outer end(mm)

$\alpha_0$  :Reference pressure angle (degree)

$\alpha_s$  :Mean transverse pressure angle (degree)  $= \tan^{-1}(\tan \alpha_n / \cos \beta_m)$

$\alpha_n$  :Reference normal pressure angle (degree)

Table 10.17 The transverse contact ratio for Gleason's straight bevel gear,  $\epsilon_\alpha (\Sigma = 90^\circ, \alpha_0 = 20^\circ)$

$\frac{z_1}{z_2}$	12	15	16	18	20	25	30	36	40	45	60
12	1.514										
15	1.529	1.572									
16	1.529	1.578	1.588								
18	1.528	1.584	1.597	1.616							
20	1.525	1.584	1.599	1.624	1.640						
25	1.518	1.577	1.595	1.625	1.650	1.689					
30	1.512	1.570	1.587	1.618	1.645	1.697	1.725				
36	1.508	1.563	1.579	1.609	1.637	1.692	1.732	1.758			
40	1.506	1.559	1.575	1.605	1.632	1.688	1.730	1.763	1.775		
45	1.503	1.556	1.571	1.600	1.626	1.681	1.725	1.763	1.781	1.794	
60	1.500	1.549	1.564	1.591	1.615	1.668	1.710	1.751	1.773	1.796	1.833

Table 10.18 The transverse contact ratio for standard straight bevel gear,  $\epsilon_\alpha (\Sigma = 90^\circ, \alpha_0 = 20^\circ)$

$\frac{z_1}{z_2}$	12	15	16	18	20	25	30	36	40	45	60
12	1.514										
15	1.545	1.572									
16	1.554	1.580	1.588								
18	1.571	1.595	1.602	1.616							
20	1.585	1.608	1.615	1.628	1.640						
25	1.614	1.636	1.643	1.655	1.666	1.689					
30	1.634	1.656	1.663	1.675	1.685	1.707	1.725				
36	1.651	1.674	1.681	1.692	1.703	1.725	1.742	1.758			
40	1.659	1.683	1.689	1.702	1.712	1.734	1.751	1.767	1.775		
45	1.666	1.691	1.698	1.711	1.721	1.743	1.760	1.776	1.785	1.794	
60	1.680	1.707	1.714	1.728	1.739	1.762	1.780	1.796	1.804	1.813	1.833

Table 10.19 The transverse contact ratio for Gleason's spiral bevel gear,  $\epsilon_\alpha (\Sigma = 90^\circ, \alpha_0 = 20^\circ, \beta_m = 35 \text{ deg})$

### (3)-4 Spiral Angle Factor, $Y_\beta$

The spiral angle factor,  $Y_\beta$ , is obtainable from Equation (10.39).

### (3)-5 Cutter Diameter Effect Factor, $Y_C$

The cutter diameter effect factor,  $Y_C$ , can be obtained from Table 10.20 by the value of tooth flank length,  $b/\cos \beta_m$  (mm),

over cutter diameter.

If cutter diameter is not known, assume  $Y_C = 1.0$ .

Table 10.20 Cutter diameter effect factor,  $Y_C$

(3)-6 Life Factor,  $K_L$

The life factor,  $K_L$ , is obtainable from Table 10.2.

(3)-7 Size Factor of Bending Stress at Root,  $K_{FX}$

The size factor of bending stress at root,  $K_{FX}$ , can be obtained from Table 10.21 based on the transverse module,  $m$ .



## Table 10.21 Size factor for bending strength, KFX

## (3)-8 Longitudinal Load Distribution Factor, KM

The longitudinal load distribution factor, KM, is obtained from Table 10.22 or Table 10.23.

Table 10.22 Longitudinal load distribution factor, KM for spiral bevel gears, zero bevel gears and straight bevel gears with

## crowning

Table 10.23 Tooth Flank Load Distribution Factor  $K_M$  for Straight Bevel Gears without Crowning

(3)-9 Dynamic Load Factor,  $K_V$   
Dynamic load factor,  $K_V$ , is a function of the precision grade of

the gear and the tangential speed at the outer pitch circle, as shown in Table 10.24.

### (3)-10 Overload Factor, $K_O$

The overload factor,  $K_O$ , can be computed from Equation (10.12) or obtained from Table 10.4, identical to the case of spur and helical gears.

### (3)-11 Reliability Factor, $K_R$

The reliability factor,  $K_R$ , should be assumed to be as follows:

1. General case  $K_R = 1.2$
2. When all other factors can be determined accurately:  $K_R = 1.0$
3. When all or some of the factors cannot be known with certainty:  $K_R = 1.4$

### (3)-12 Allowable Bending Stress at Root, $\sigma_{Flim}$

The allowable bending stress at the root is obtained by a bending strength calculation for spur and helical gears as shown at < (3)-10 >.

## (4) Example of Calculation

## Gleason straight bevel gear design details

Bending strength factors for Gleason straight bevel gear

Related links:

[Strength and Durability of Gears](#) – A page of The ABC's of Gears / Basic Guide – B

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